

TECHNICAL MANUAL

TTECHS R6

Wastewater Technical Manual

FOR GOULDS WATER TECHNOLOGY, BELL & GOSSETT, RED JACKET SERIES AND CENTRIPRO

Goulds Water Technology, Bell & Gossett, Red Jacket Series, CentriPro

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Wastewater

FRICTION LOSS

PLASTIC PIPE: FRICTION LOSS (IN FEET OF HEAD) PER 100 FT.

6014	6.011	3⁄8"	1⁄2"	3⁄4"	1"	1¼"	1½"	2"	2½ "	3"	4"	6"	8"	10"
GPM	GPH	ft.	ft.	ft.	ft.	ft.	ft.							
1	60	4.25	1.38	.356	.11									
2	120	15.13	4.83	1.21	.38	.10								
3	180	31.97	9.96	2.51	.77	.21	.10							
4	240	54.97	17.07	4.21	1.30	.35	.16							
5	300	84.41	25.76	6.33	1.92	.51	.24							
6	360		36.34	8.83	2.69	.71	.33	.10						
8	480		63.71	15.18	4.58	1.19	.55	.17						
10	600		97.52	25.98	6.88	1.78	.83	.25	.11					
15	900			49.68	14.63	3.75	1.74	.52	.22					
20	1,200			86.94	25.07	6.39	2.94	.86	.36	.13				
25	1,500				38.41	9.71	4.44	1.29	.54	.19				
30	1,800					13.62	6.26	1.81	.75	.26				
35	2,100					18.17	8.37	2.42	1.00	.35	.09			
40	2,400					23.55	10.70	3.11	1.28	.44	.12			
45	2,700					29.44	13.46	3.84	1.54	.55	.15			
50	3,000						16.45	4.67	1.93	.66	.17			
60	3,600						23.48	6.60	2.71	.93	.25			
70	4,200							8.83	3.66	1.24	.33			
80	4,800							11.43	4.67	1.58	.41			
90	5,400							14.26	5.82	1.98	.52			
100	6,000								7.11	2.42	.63	.08		
125	7,500								10.83	3.80	.95	.13		
150	9,000									5.15	1.33	.18		
175	10,500									6.90	1.78	.23		
200	12,000									8.90	2.27	.30		
250	15,000										3.36	.45	.12	
300	18,000										4.85	.63	.17	
350	21,000										6.53	.84	.22	
400	24,000											1.08	.28	
500	30,000											1.66	.42	.14
550	33,000											1.98	.50	.16
600	36,000											2.35	.59	.19
700	42,000												.79	.26
800	48,000												1.02	.33
900	54,000												1.27	.41
950	57,000													.46
1000	60,000													.50

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FRICTION LOSS

STEEL PIPE: FRICTION LOSS (IN FEET OF HEAD) PER 100 FT.

		3⁄8"	1⁄2"	3⁄4 "	1"	1¼"	1½"	2"	2 ½"	3"	4"	5"	6"	8"	10"
GPM	GPH	ft.	ft.	ft.	ft.	ft.	ft.	ft.							
1	60	4.30	1.86	.26											
2	120	15.00	4.78	1.21	.38										
3	180	31.80	10.00	2.50	.77	.10									
4	240	54.90	17.10	4.21	1.30	.34									
5	300	83.50	25.80	6.32	1.93	.51	.24								
6	360		36.50	8.87	2.68	.70	.33	.10							
7	420		48.70	11.80	3.56	.93	.44	.13							
8	480		62.70	15.00	4.54	1.18	.56	.17							
9	540			18.80	5.65	1.46	.69	.21							
10	600			23.00	6.86	1.77	.83	.25	.11	.04					
12	720			32.60	9.62	2.48	1.16	.34	.15	.05					
15	900			49.70	14.70	3.74	1.75	.52	.22	.08					
20	1,200			86.10	25.10	6.34	2.94	.87	.36	.13					
25	1,500				38.60	9.65	4.48	1.30	.54	.19					
30	1,800				54.60	13.60	6.26	1.82	.75	.26					
35	2,100				73.40	18.20	8.37	2.42	1.00	.35					
40	2,400				95.00	23.50	10.79	3.10	1.28	.44					
45	2,700					30.70	13.45	3.85	1.60	.55					
70	4,200					68.80	31.30	8.86	3.63	1.22	.35				
100	6,000						62.20	17.40	7.11	2.39	.63				
150	9,000							38.00	15.40	5.14	1.32	.08			
200	12,000							66.30	26.70	8.90	2.27	.736	.30	.08	
250	15,000							90.70	42.80	14.10	3.60	1.20	.49	.13	
300	18,000								58.50	19.20	4.89	1.58	.64	.16	.0542
350	21,000								79.20	26.90	6.72	2.18	.88	.23	.0719
400	24,000								103.00	33.90	8.47	2.72	1.09	.279	.0917
450	27,000								130.00	42.75	10.65	3.47	1.36	.348	.114
500	30,000								160.00	52.50	13.00	4.16	1.66	.424	.138
550	33,000								193.00	63.20	15.70	4.98	1.99	.507	.164
600	36,000								230.00	74.80	18.60	5.88	2.34	.597	.192
650	39,000									87.50	21.70	6.87	2.73	.694	.224
700	42,000									101.00	25.00	7.93	3.13	.797	.256
750	45,000									116.00	28.60	9.05	3.57	.907	.291
800	48,000									131.00	32.40	10.22	4.03	1.02	.328
850	51,000									148.00	36.50	11.50	4.53	1.147	.368
900	54,000									165.00	40.80	12.90	5.05	1.27	.410
950	57,000									184.00	45.30	14.30	5.60	1.41	.455
1000	60,000									204.00	50.20	15.80	6.17	1.56	.500

Wastewater

FRICTION LOSS

EQUIVALENT NUMBER OF FEET STRAIGHT PIPE FOR DIFFERENT FITTINGS

Size of fittings, Inches	1⁄2"	3⁄4"	1"	1¼"	11⁄2"	2"	2 ½"	3"	4"	5"	6"	8"	10"
90° Ell	1.5	2.0	2.7	3.5	4.3	5.5	6.5	8.0	10.0	14.0	15	20	25
45° Ell	0.8	1.0	1.3	1.7	2.0	2.5	3.0	3.8	5.0	6.3	7.1	9.4	12
Long Sweep Ell	1.0	1.4	1.7	2.3	2.7	3.5	4.2	5.2	7.0	9.0	11.0	14.0	
Close Return Bend	3.6	5.0	6.0	8.3	10.0	13.0	15.0	18.0	24.0	31.0	37.0	39.0	
Tee-Straight Run	1	2	2	3	3	4	5						
Tee-Side Inlet or Outlet or Pitless Adapter	3.3	4.5	5.7	7.6	9.0	12.0	14.0	17.0	22.0	27.0	31.0	40.0	
Ball or Globe Valve Open	17.0	22.0	27.0	36.0	43.0	55.0	67.0	82.0	110.0	140.0	160.0	220.0	
Angle Valve Open	8.4	12.0	15.0	18.0	22.0	28.0	33.0	42.0	58.0	70.0	83.0	110.0	
Gate Valve-Fully Open	0.4	0.5	0.6	0.8	1.0	1.2	1.4	1.7	2.3	2.9	3.5	4.5	
Check Valve (Swing)	4	5	7	9	11	13	16	20	26	33	39	52	65
In Line Check Valve (Spring) or Foot Valve	4	6	8	12	14	19	23	32	43	58			

Example:

(A) 100 ft. of 2" plastic pipe with one (1) 90° elbow and one (1) swing check valve.

90° elbow - equivalent to	5.5 ft. of straight pipe
Swing check - equivalent to	13.0 ft. of straight pipe
5	
100 ft. of pipe - equivalent to	100 ft. of straight pipe
	110E(T. I

t. of straight pipe of straight pipe

118.5 ft. = Total equivalent pipe

Figure friction loss for 118.5 ft. of pipe.

PIPE VOLUME AND VELOCITY

STORAGE OF WATER IN VARIOUS SIZE PIPES

Pipe Size	Volume in Gallons per Foot	Pipe Size	Volume in Gallons per Foot
11⁄4	.06	6	1.4
1½	.09	8	2.6
2	.16	10	4.07
3	.36	12	5.87
4	.652		

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(B) Assume flow to be 80 GPM through 2" plastic pipe.

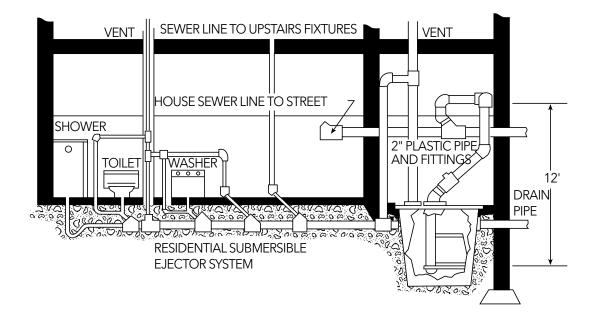
- 1. Friction loss table shows 11.43 ft. loss per 100 ft. of pipe.
- 2. In step (A) above we have determined total ft. of pipe to be 118.5 ft.
- 3. Convert 118.5 ft. to percentage 118.5 ÷ 100 = 1.185 4. Multiply 11.43
- - x 1.185
 - 13.54455 or 13.5 ft. = Total friction loss in this system.

Pipe Size	Minimum GPM	Pipe Size	Minimum GPM
11⁄4	9	6	180
1½	13	8	325
2	21	10	500
3	46	12	700
4	80		

MINIMUM FLOW TO MAINTAIN 2FT./SEC. ***SCOURING VELOCITY IN VARIOUS PIPES**

* Failure to maintain or exceed this velocity will result in clogged pipes. Based on schedule 40 nominal pipe.

SEWAGE PUMP SELECTION



The primary function for which the Submersible Sewage Pump is designed is the handling of sewage and other fluids containing unscreened nonabrasive solids and wastes. In order to insure a maximum of efficiency and dependable performance, careful selection of pump size is necessary. Required pump capacity will depend upon the number and type of fixtures discharging into the sump basin, plus the type of facility served. The fundamentals involved in selecting a pump for a Water System can be applied to selecting a Submersible Sewage Pump. By answering the three (3) questions concerning capacity, suction, and discharge conditions we will know what is required of the pump and be able to select the right pump from the catalog.

1. To simplify the selection of the proper size Submersible Sewage Pump, the general rule is to base the pump capacity on the number of toilets the pump will be serving. This differs from the selection of the proper pump for a Water System in that question 1, "Water Needed" is reversed. How much liquid do we want to dispose of rather than how much do we need? The following chart will help determine pump capacity:

Sewage Selection Table for Residential or Commercial Systems

Number of Bathrooms	GPM
1	20
2	30

The above selection table takes into consideration other fixtures which will drain only water into the sewage basin.

Therefore, pump capacity should not be increased for lavatories, bathtubs, showers, dishwashers, or washing machines. When no toilets are involved in the facility served, for example, a laundromat, the major fixture discharging waste should be considered. In this case, the chart should read "Maximum Number of Washing" Machines."

In areas where drain tile from surrounding lawns or fields enters the sump, groundwater seepage can be determined as follows:

14 GPM for 1,000 sq. ft. of sandy soil 8 GPM for 1,000 sq. ft. of clay soil

If the calculated groundwater seepage is less than one-fourth of the pump capacity required based on the number of toilets, the pump capacity should not be increased. Any seepage over the allowed onefourth should be added to the required pump capacity.

- **2.** Since the pump is submerged in the liquid to be pumped, there is no suction lift. Question 2 does NOT become a factor in pump selection.
- **3.** Answering Question 3, discharge conditions is the final step in selecting a Submersible Sewage Pump. Only the vertical distance between the pump and the highest point in the discharge piping, plus friction losses in discharge pipe and fittings affect discharge pressure. (Friction losses can be obtained from the friction table in this Selection Manual.)

Normally service pressure is not a consideration. The total of the vertical distance, plus the friction losses is the required discharge head in feet.

Wastewater

WASTEWATER PUMPS SIZING AND SELECTION

WHAT DO YOU NEED TO KNOW TO SELECT A SEWAGE PUMP?

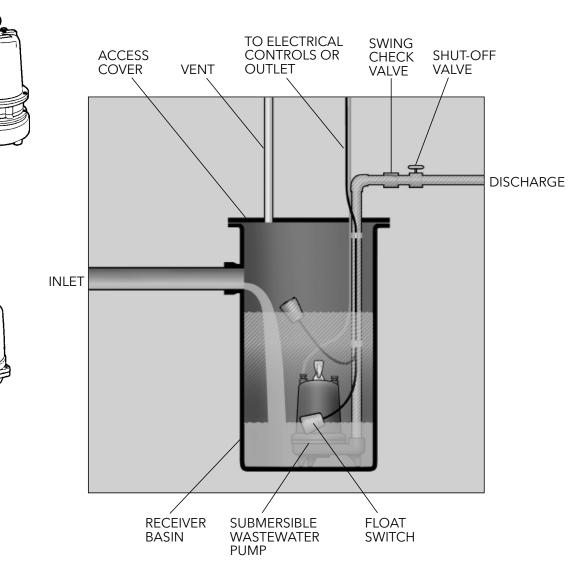
1. Size solids to be handled.

- Effluent (liquid only) <1"
- Residential 1½" or larger
- Commercial/Industrial 21/2" or larger

2. Capacity required.

- 1 bath 20 GPM
- 2-3 baths 30 GPM
- 4-5 baths 45 GPM

3. Pump/Motor Run Time Units up to 1½ HP should run a minimum of 1 minute. Two (2) HP and larger units should run a minimum of 2 minutes.





4. Formula for Total Dynamic Head:

Vertical elevation + friction loss (pipe + fittings) + Pressure Requirements (x 2.31')

Total head in feet

Note: Wastewater pumps are designed to pump effluent with some suspended solids, not solids with some effluent.

5. Must maintain minimum velocity of 2 ft./second (see index).

6. Must turn storage in the discharge pipe a **minimum** of one time per cycle. (See index).

7. Are receiver basin and cover required?

8. What is the power available?

- Phase 1Ø or 3Ø
- Voltage 115, 200, 230, 460 or 575 V
- Hertz 50 or 60 Hz

9. What pipe size will be used?

10. Simplex or Duplex System?

(Duplex when service cannot be interrupted)

Note: State and local codes take preference.

FLOW RATE CALCULATION

Residential Sizing

BATHROOM COUNT

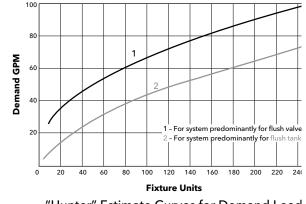
Number of Bathrooms	Flow Rate per Minute
1	20
2	30
3	40
4	50
5	60
6	70

FIXTURE COUNT V = Value style fixture T = Tank Style Fixture

Fixture	Туре	Count	
Toilet	V	6	
Toilet	Т	3	
Lav Sink	V or T	1	
Tub	V or T	2	
Shower	V or T	2	
Full Body Shower	Add Flow rate: 9 to 65 Gallons per minute to total		
Kitchen Sink	V or T	2	
Dishwasher	V or T	4	
Wash Machine	V or T	8	
Bidet	V or T	3	
Icemaker	V or T	3	
Hose Bib	VorT	4	

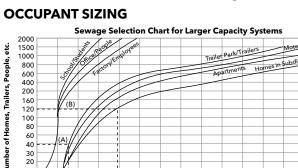
Fixture	Quantity	Count	Total Count
Toilets	3	3	9
Tub and Shower	2	4	8
Full body shower			15
Lav Sink		1	3
Kitchen Sink	1	2	2
Dishwasher	1	4	4
lcemaker	1	3	3
Wash Machine	1	8	8
Hose Bib	1	4	4
Total			56

PLUMBING WATER SYSTEMS

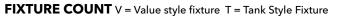


"Hunter" Estimate Curves for Demand Load PAGE 8

Commercial Sizing



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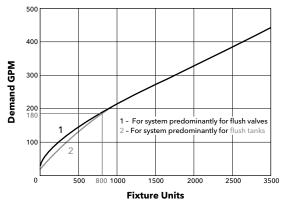


100 150 200 250 300 350 400 500 600 700 800 900 1000

Fixture	Туре	Count	
Toilet	V	10	
Toilet	Т	5	
Pedestal Urinal	V or T	10	
Stall Urinal	V or T	5	
Lav Sink	V or T	3	
Kitchen Sink	V or T	4	
Tub	V or T	4	
Shower	V or T	4	
Dishwasher	V or T	4	
Icemaker	V or T	3	
Commercial Wash. Machine	V or T	6	
Hose Bib - Commercial	V or T	6	
Full Body Shower	Add Flow rate 9 to 65 Gallons per minute to total		

Fixture	Quantity	Count	Total Count
Toilet	50	10	500
Lav Sink	50	3	150
Shower	50	4	200
Full body shower	50	15	750
Dishwasher	50	4	200
lcemaker	50	3	150
Wash Machine	10	6	60
Dishwasher	10	4	40
Hose bib	2	6	12
Total			2062

PLUMBING WATER SYSTEMS



"Hunter" Estimate Curves for Demand Load

Wastewater

FLOW CALCULATION EXAMPLE

To Calculate Flow with Fixture Counts

Take total number of each style fixture X Count for that fixture. Add all fixture total counts. Add Full Body shower flow rate to total.

Use "Hunter" estimate curves for Demand Load for appropriate style fixtures. (Valve style fixtures are predominant in Commercial buildings; Tank style fixtures are predominant in Residential).

COMMERCIAL BUILDING EXAMPLE:

Valve Style Fixtures

25 Toilets 25 Lav sinks 25 Tubs 6 Kitchen Sinks 2 Commercial Washing Machines 1 Dishwasher

HEAD CALCULATION

Example: Fig. 1. A two-bathroom home is situated such that the city sewer main is located above the basement drain facilities. Groundwater seepage through drain tile into the sump is estimated at 6 GPM. The vertical distance from the pump to the highest point in the discharge piping is 12 feet.

A pump capable of pumping 30 GPM is required (seepage is less than one-fourth of the pump capacity so it is automatically included). The discharge head must be 12 feet, plus any friction loss in the approximately 15 feet of pipe, 3-90° elbows, 3-45° elbows, and check valve. Assume plastic pipe is used.

1. RATE OF FLOW = 30 GPM

Two (2) toilets, includes seepage up to one-fourth of selected _____ pump capacity. 6 GPM is less than the 7.5 GPM allowable so no correction is necessary.

2. SUCTION CONDITIONS - Flooded Suction

3. DISCHARGE CONDITIONS

Vertical Differential 12.0'

- Friction losses @ 30 GPM
- 15' of 2" pipe (1.8' per 100' of pipe) = .2' F.L.
- $3-2", 90^{\circ}$ elbows = 16.5 equivalent feet $3-2^{"}, 45^{\circ}$ elbows = 7.5 equivalent feet
- 1-check valve = 19.0 equivalent feet
- Total = 43.0 equivalent feet = .6' F.L.

Total Discharge Head =

Referring to the catalog, we find that a $1/_3$ HP Sewage Pump should be adequate for the job.

12.8'

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25 Toilets X 10 Count 250 = 25 Lav Sinks X 3 Count = 75 25 Tubs X 4 Count = 100 6 Kitchen Sinks X 4 Count 24 = 2 Commercial X 6 Count = 12 1 Dishwasher X 4 Count = 4 465 Count Total **Plumbing Water Systems** antly for flush valve For system predor For system predo ninantly for Fixture Units

Count Calculation

"Hunter" Estimate Curves for Demand Load

Example: The same conditions as in the previous example exist, except the house is located on a large tract of sandy soil where the groundwater seepage is estimated @ 20 GPM.

1. RATE OF FLOW = 30 GPM

Two (2) toilets, includes seepage up to one-fourth of selected pump capacity - 7.5 GPM. The additional 12.5 GPM (20-7.5) must be added to the required pump capacity -12.5 GPM **Total** = 42.5 GPM 2. SUCTION CONDITIONS Flooded Suction **3. DISCHARGE CONDITIONS** Vertical Differential - 12.0' Friction losses @ 42.5 GPM 15' of 2" pipe (3.5' per 100' of pipe) = .5' F.L. 3-2", 90° elbows = 16.5 equivalent feet $3-2", 45^{\circ}$ elbows = 7.5 equivalent feet 1-check valve = 19.0 equivalent feet Total = 43.0 equivalent feet or 1.5' F.L.

Total Discharge Head = 14.0'

Referring again to the catalog, we find that a $1/_3$ HP Sewage Pump should be adequate for this installation. Volumes

CHART A

Dimensions

BASIN SIZING

CALCULATING BASIN SIZE

1. Choosing Diameter

A minimum of 24" is required for simplex. Duplex stations normally start at 36", but require much larger for larger diameter discharge pumps.

For example: A pump that flows 100 GPM, requires a 2-minute run time. A duplex station with a diameter of 36" holds 4.4 gallons (see Chart A) per inch.

50 GPM x 2 minutes = 100 gallons

100 gallons / 4.4 gallons per inch 22.72" for pump down.

22.72" would be used for (E).

2. Sizing Depth

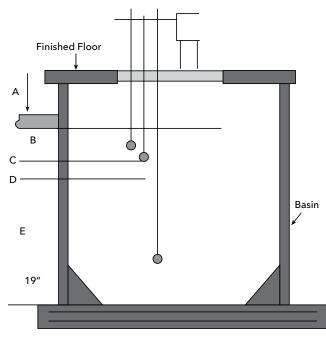
Inlet and Float Location Basin Sizing Method

1. Top of basin to bottom of the inlet (A)+	in
2. Inlet to "Alarm" float (B)	+	in
3. "Alarm" to "Lag" float (C)	+	in
4. "Lag" to "On" float (D)	+	in
5. Pump down (E) (Note A)	+	17.86 in

6. Floor of basin to top of pump case + 19.0 in. (Note B)

Note A = Minimum suggested basin diameter for duplex configuration is 36". Volume by inch of basin divided by 2 x's pumping rate.

Note B = Most pumps are approximately 19" tall. Pump should remain covered during pumping.



Diameter	Depth	Total Gallons	Gallons Per Inch
	36	65	1.81
	48	84	1.75
24	60	102	1.70
24	72	118	1.64
	84	165	1.96
	96	188	1.96
	36	110	3.00
	48	137	2.85
20	60	169	2.82
30	72	199	2.76
	84	257	3.05
	96	294	3.06
	36	159	4.41
	48	200	4.17
24	60	246	4.10
36	72	291	4.04
	84	370	4.40
	96	423	4.40
	48	274	5.71
	60	339	5.65
42	72	402	5.58
	84	504	6.00
	96	576	6.00
	48	361	7.52
	60	446	7.43
48	72	529	7.34
	84	658	7.83
	96	752	7.83
	78	955	12.24
60	84	1028	12.23
	96	1175	12.23
	78	1375	17.62
72	84	1481	17.63
	96	1692	17.63

Wastewater

ELECTRICAL DATA

AGENCY LISTINGS AND POWER CORD PLUG REMOVAL

Our single-phase sump, effluent and sewage pumps with 115, 208 and 230 volt motors up to and including 1 HP are now built with NEMA three-prong grounding plug power cords. This allows qualified electricians or professional pump installers to easily connect the pumps; according to U.S. National (NEC), Canadian (CSA), state, provincial and local electrical codes, to a properly rated piggyback float switch for automatic operation.

NOTICE: This statement is written for the intent purpose of verifying to electrical inspectors that according to both UL and CSA standards it is allowable to remove the plug ends for direct wiring to a disconnect switch, control panel or hard wired float switch. Removing the plug end does not violate our UL Listin or CSA/CUS certification in any way. Always follow the aforementioned codes when making connections to the bare leads once the plug is removed. Plug remov al information and wiring diagrams may be found in the Installation Manual supplied with the pump and in this booklet. Please use this statement in the event ar inspector needs written assurance of this policy.

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TRANSFORMER SIZES

A full three phase supply is recommended for all three phase motors, consisting of three individual transformers or one three phase transformer. "Open" delta or wye connections using only two transformers can be used, but are more likely to cause problems from current unbalance.

Transformer ratings should be no smaller than listed in the table for supply power to the motor alone.

Submersible	Total		VA Rating - nsformer
3Ø Motor HP Rating	Effective KVA Required	Open WYE DELTA 2 Transformers	WYE or DELTA 3 Transforme
11⁄2	3	2	1
2	4	2	1½
3	5	3	2
5	71⁄2	5	3
71⁄2	10	71⁄2	5
10	15	10	5
15	20	15	71⁄2
20	25	15	10
25	30	20	10
30	40	25	15
40	50	30	20
50	60	35	20
60	75	40	25

90

120

50

65

75

100

TRANSFORMER CAPACITY REQUIRED FOR CURMERCIPIE MOTORS

30

40

APPLICATION - THREE PHASE UNBALANCE

THREE PHASE POWER UNBALANCE

A full three phase supply is recommended for all three phase motors, consisting of three individual transformers or one three phase transformer. Socalled "open" delta or wye connections using only two transformers can be used, but are more likely to cause problems, such as poor performance overload tripping or early motor failure due to current unbalance. Transformer ratings should be no smaller than listed in Table 2 on page 3 for supply power to the motor alone.

Checking and correcting rotation and current unbalance

- 1. Establish correct motor rotation by running in both directions. Change rotation by exchanging any two of the three motor leads. The rotation that gives the most water flow is always the correct rotation.
- 2. After correct rotation has been established, check the current in each of the three motor leads and calculate the current unbalance as explained in 3 below.

If the current unbalance is 2% or less, leave the leads as connected.

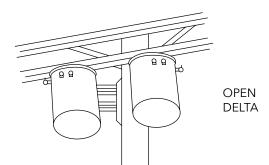
If the current unbalance is more than 2%, current readings should be checked on each leg using each of the three possible hook-ups. Roll the motor leads across the starter in the same direction to prevent motor reversal.

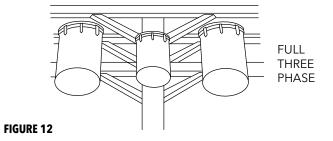
- 3. To calculate percent of current unbalance:
- A. Add the three line amp values together.
- B. Divide the sum by three, yielding average current.
- C. Pick the amp value which is furthest from the average current (either high or low).
- D. Determine the difference between this amp value (furthest from average) and the average.
- E. Divide the difference by the average. Multiply the result by 100 to determine percent of unbalance.
- 4. Current unbalance should not exceed 5% at service factor load or 10% at rated input load. If the unbalance cannot be corrected by rolling leads, the source of the unbalance must be located and corrected. If, on the three possible hookups, the leg farthest from the average stays on the same power lead, most of the unbalance is coming from the power source. However, if the reading farthest from average moves with the same motor lead, the primary source of unbalance is on the "motor side" of the starter. In this instance, consider a damaged cable, leaking splice, poor connection, or faulty motor winding.

Phase designation of leads for CCW rotation viewing shaft end

To reverse rotation, interchange any two leads. Phase 1 or "A" - Black Motor Lead or T1 Phase 2 or "B" - White Motor Lead or T2 Phase 3 or "C" - Red Motor Lead or T3 **Notice:** Phase 1, 2 and 3 may not be L1, L2 and L3.

Starter Terminals	Ho L1 ⊥ ⊤ T1	ookup L2 ⊥ T T2	0 1 L3 ⊥ ⊤ T3	H L1 ⊥ ⊤ T1	ookup L2 ⊥ T T2	2 L3 ⊥ ⊤ T3	H₁ L1 ⊥ ⊤ T1	ookup L2 上 T T2) 3 L3 ⊥ ⊤ T3
Motor									
Leads	R	В	W	W	R	В	В	W	R
	Т3	T1	T2	Т2	Т3	T1	T1	T2	Т3
Example:									
- т	- 3-R =	51 ar	nps	T2-W =	= 50 a	mps	T1-B	= 50 a	mps
Т	1-B =	46 ar	nps	T3-R =	= 48 a	mps	T2-W	= 49 a	mps
T:	2-W =	53 ar	nps	T1-B =	= 52 a	mps	T3-R	= 51 a	mps
То	tal = 1	1 <u>50 a</u> r	nps	Total =	150 a	mps	Total =	150 a	mps
	÷ 3 =	50 ar	nps	÷ 3 =	= 50 a	mps	÷ 3	= 50 a	mps
-46 = 4 amps		-48 = 2 amps		mps	– 49 = 1 amps				
4 ÷	50 =	.08 or	8%	2 ÷ 50 =	.04 o	r 4%	1 ÷ 50 =		





Wastewater

ELECTRICAL DATA

NEMA CONTROL PANEL ENCLOSURES

Enclosure Rating	Explanation
NEMA 1 ①	To prevent accide
General Purpose	application indoo
NEMA 2	To prevent accide
Driptight	or dirt.
NEMA 3 ①	Protection against
Weatherproof	
(Weatherproof Resistant)	
NEMA 3R ①	Protects against e
Raintight	outdoor application
NEMA 4 ①	Designed to exclu
Watertight	against stream of
NEMA 4X ①	Designed to exclu
Watertight & Corrosion Resistant	against stream of
NEMA 5	Constructed so th
Dust Tight	some equipment
NEMA 6	Intended to perm
Submersible	submerged in wat
NEMA 7	Designed to meet
Hazardous Locations	Class 1, Hazardou
Class I - Air Break	occurs in air.
NEMA 8	Identical to NEMA
Hazardous Locations	
A, B, C or D	
Class II - Oil Immersed	
NEMA 9	Designed to meet
Hazardous Locations	Class II Hazardous
E, F or G	
Class II	
NEMA 10	Meets requiremer
Bureau of Mines	
Permissible	
NEMA 11	Provides oil imme
Dripproof	where equipment
Corrosion Resistant	
NEMA 12	For use in those in
Driptight, Dusttight	and flyings, or oil

① Types available from Xylem, Residential and Commercial Water.

ental contact with enclosed apparatus. Suitable for ors where not exposed to unusual service conditions. ental contact, and in addition, to exclude falling moisture

st specified weather hazards. Suitable for use outdoors.

entrance of water from a beating rain. Suitable for general ion not requiring sleetproof.

ude water applied in form of hose stream. To protect water during cleaning operations, etc.

ude water applied in form of hose stream. To protect water during cleaning operations, etc. Corrosion Resistant. nat dust will not enter enclosed case. Being replaced in by NEMA 12.

nit enclosed apparatus to be operated successfully when ater under specified pressure and time.

et application requirements of National Electrical Code for us Locations (explosive atmospheres). Circuit interruption

A 7 above, except the apparatus is immersed in oil.

et application requirements of National Electrical Code for is Locations (combustible dusts, etc.).

ents of U.S. Bureau of Mines. Suitable for use in coal mines.

ersion of apparatus such that it is suitable for application It is subject to acid or other corrosive fumes.

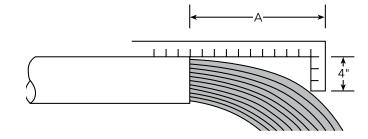
ndustries where it is desired to exclude dust, lint, fibers or Industrial coolant seepage.

DETERMINING FLOW RATES

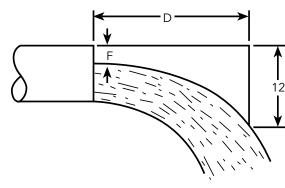
FULL PIPE FLOW - CALCULATION OF DISCHARGE RATE USING HORIZONTAL OPEN DISCHARGE FORMULA

An L-shaped measuring square can be used to estimate flow capacity, using the chart below. As shown in illustration, place 4" side of square so that it hangs down and touches the water. The horizontal distance shown "A" is located in the first column of the chart and you read across to the pipe diameter (ID) to find the gallons per minute discharge rate.

Example: A is 8" from a 4" ID pipe = a discharge rate of 166 GPM.



PIPE NOT RUNNING FULL - CALCULATION OF DISCHARGE RATE USING AREA FACTOR METHOD



-	Flow (GPM) = $A \times D \times 1.093 \times F$ A = Area of pipe in square inches D = Horizontal distance in inches F = Effective area factor from chart Area of pipe equals inside Dia. ² x 0.7854
- -	Example: Pipe inside diameter = 10 in. D = 20 in. F = 2½ in. A = 10 x 10 x 0.7854 = 78.54 square in. R % = $\frac{F}{D} = \frac{2½}{10} = 25\%$ F = 0.805 Flow = 78.54 x 20 x 1.039 x 0.805 = 1314 GPM

Ratio F/D = R %	Eff. Area Factor F	Ratio F/D = R %	Eff. Area Factor F
5	0.981	55	0.436
10	0.948	60	0.373
15	0.905	65	0.312
20	0.858	70	0.253
25	0.805	75	0.195
30	0.747	80	0.142
35	0.688	85	0.095
40	0.627	90	0.052
45	0.564	95	0.019
50	0.500	100	0.000

Flow From Horizontal Pipe (Not Full)

DISCHARGE RATE IN GALLONS PER MINUTE/NOMINAL PIPE SIZE (ID)

Horizontal						I Pipe Diameter						
Dist. (A) Inches	1"	1¼"	1½"	2"	21⁄2"	3"	4"	5"	6"	8"	10"	12"
4	5.7	9.8	13.3	22.0	31.3	48.5	83.5					
5	7.1	12.2	16.6	27.5	39.0	61.0	104	163				
6	8.5	14.7	20.0	33.0	47.0	73.0	125	195	285			
7	10.0	17.1	23.2	38.5	55.0	85.0	146	228	334	380		
8	11.3	19.6	26.5	44.0	62.5	97.5	166	260	380	665	1060	
9	12.8	22.0	29.8	49.5	70.0	110	187	293	430	750	1190	1660
10	14.2	24.5	33.2	55.5	78.2	122	208	326	476	830	1330	1850
11	15.6	27.0	36.5	60.5	86.0	134	229	360	525	915	1460	2100
12	17.0	29.0	40.0	66.0	94.0	146	250	390	570	1000	1600	2220
13	18.5	31.5	43.0	71.5	102	158	270	425	620	1080	1730	2400
14	20.0	34.0	46.5	77.0	109	170	292	456	670	1160	1860	2590
15	21.3	36.3	50.0	82.5	117	183	312	490	710	1250	2000	2780
16	22.7	39.0	53.0	88.0	125	196	334	520	760	1330	2120	2960
17		41.5	56.5	93.0	133	207	355	550	810	1410	2260	3140
18			60.0	99.0	144	220	375	590	860	1500	2390	3330
19				110	148	232	395	620	910	1580	2520	3500
20					156	244	415	650	950	1660	2660	3700
21						256	435	685	1000	1750	2800	
22							460	720	1050	1830	2920	
23							ĺ	750	1100	1910	3060	
24									1140	2000	3200	

Wastewater

TERMS AND USABLE FORMULAS

The term "head" by itself is rather misleading. It is commonly taken to mean the difference in elevation between the suction level and the discharge level of the liquid being pumped. Although this is partially correct, it does not include all of the conditions that should be included to give an accurate description.

fittings.

Friction Head: The pressure expressed in lbs./sq. in. or feet of liquid needed to overcome the resistance to the flow in the pipe and

source. Static Suction Head: The vertical distance from the center line of the pump up to the free level of the liquid

Suction Lift: Exists

when the source of

supply is below the

center line of the

■ Suction Head: Ex-

ists when the source

the center line of the

The vertical distance

from the center line of

of supply is above

■ Static Suction Lift:

pump.

pump.

source. Static Discharge Head:

BASIC FORMULAS AND SYMBOLS Formulas

Formula	d5	
GPM=	Lb./Hr.	$BHP = GPM \times H \times Sp. Gr.$
	500 x Sp. Gr.	3960 x Eff.
H =	2.31 x psi Sp. Gr.	Eff. = $\frac{\text{GPM x H x Sp. Gr.}}{20(0 - \text{DHP})}$
	Sp. 01.	3960 x BHP
H =	1.134 x ln. Hg.	N _s = N√GPM
	Sp. Gr.	H ^{3/4}
H _v =	$V^2 = 0.155 V^2$	$H = V^2$
	2g	2g
V = GF	$PM \times 0.321 = GPM \times 0.409$	
	A (I.D.) ²	

Symbo	ols				
GPM	=	gallons per minute	g	=	32.16 ft.
Lb.	=	pounds	Α	=	area in s
Hr.	=	hour	ID	=	inside d
Sp. Gr.	=	specific gravity	BHP	=	brake ho
н	=	head in feet	Eff.	=	pump et
psi	=	pounds per square inch	Ns	=	specific
In. Hg.	=	inches of mercury	N	=	speed ir
h	=	velocity head in feet	D	=	impeller
v	=	velocity in feet per second			

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> The vertical elevation from the center line of the pump to the point of free discharge.

- Dynamic Suction Lift: Includes static suction lift, friction head loss and velocity head.
- Dynamic Suction Head: Includes static suction head minus friction head minus velocity head.
- the pump down to the ■ Dynamic Discharge free level of the liquid Head: Includes static discharge head plus friction head plus velocity head.
 - Total Dynamic Head:

Includes the dynamic discharge head plus dynamic suction lift or minus dynamic suction head.

■ Velocity Head: The head needed to accelerate the liquid. Knowing the velocity of the liquid, the velocity head loss can be calculated by a simple formula Head = $V^2/2g$ in which g is acceleration due to gravity or 32.16 ft./sec. Although the velocity head loss is a factor in figuring the dynamic heads, the value is usually small and in most cases negligible. See table.

Motor HP	or cost base	owatts input ed on 1 cent vatt hour	Motor HP	*Av. kw input or cost per hr. based on 1 cent per kw hour	
	1 Phase 3 P			3 Phase	
1/3	.408		20	16.9	
1⁄2	.535	.520	25	20.8	
3⁄4	.760	.768	30	26.0	
1	1.00	.960	40	33.2	
11⁄2	1.50	1.41	50	41.3	
2	2.00	1.82	60	49.5	
3	2.95	2.70	75	61.5	
5	4.65	4.50	100	81.5	
7½	6.90	6.75	125	102	
10	0.20	0.00	150	122	
10	9.30	9.00	200	162	

Approximate Cost of Operating Electric Motors

t./sec.² (acceleration of gravity)

- square inches (πr^2) (for a circle or pipe)
- diameter in inches
- orsepower
- efficiency expressed as a decimal
- speed
- in revolutions per minute
- er in inches

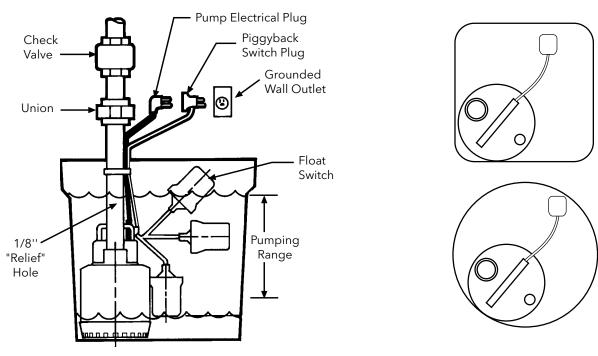
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Wastewater

TERMS AND USABLE FORMULAS BASIC FORMULAS AND SYMBOLS

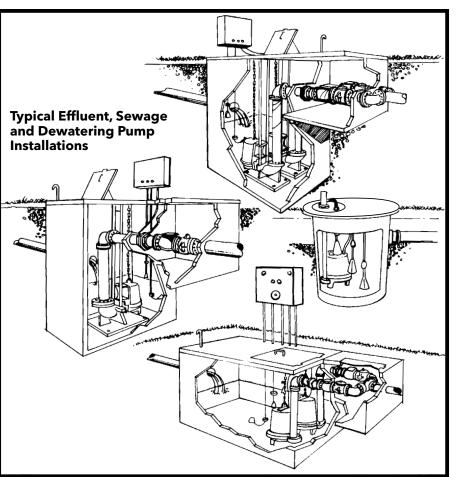
Temperature co	onversion	\frown	Area of a Circle		
		(
	(DEG. F - 32) x .555	$\left(d \left(r \right) \right)$	A = area; C = circumference.		
DEG.F =	(DEG. C x 1.8) + 32	ХУ	$A = \pi r^2; \pi = 3.14$	r = radius	
		CIRCLE	$C = 2\pi r$		
Water Horsepowe	$r = \frac{\text{GPM x 8.33 x Head}}{33000} = \frac{\text{GP}}{23000}$	M x Head 3960	Where:GPM= Gallons per Minute8.33= Pounds of water per gallon33000= Ft. Lbs. per minute in one horsHead= Difference in energy head in fermion	epower eet (field head).	
Laboratory BHP =	=Head x GPM x Sp. Gr.		Where:		
	3960 x Eff.		GPM = Gallons per Minute		
Field BHP = Lab	ooratory BHP + Shaft Loss		Head = Lab. Head (including column lo Eff. = Lab. Eff. of Pump Bowls	DSS)	
fotal BHP = Field	d BHP + Thrust Bearing Loss		Shaft Loss = HP loss due to mechanical fr		
			Thrust Bearing Loss = HP Loss in driver th (See (1) below unc		
Input Horsepower	r = Total BPH		Motor Eff. from Motor mfg. (as a decimal)		
	Motor Eff.				
Field Efficiency =	=Water Horsepower		Water HP as determined above		
	Total BHP		Total BHP as determined above		
Overall Plant Effic	ciency = Water Horsepower		(See (2) below under Misc.)		
	Input Horsepower		Water HP as determined above Input HP as determined above		
	Input Horsepower = BHP =	= 4.826 x K x M x R = 1.	732 x E x I x PF		
	Mot. Eff.		746		
	ВНР	= Brake Horsepowe	er as determined above		
		 Rated Motor Effic 	iency		
	K	= Power Company	Meter Constant Mater Multiplier, or Patia of Current and Pate	untial	
M = Power Company Meter Multiplier, or Ratio of Current and Potential					
	M			intidi	
Flectrical	R		nected with meter	inta	
Electrical	R T	Transformers con = Revolutions of me = Time in Sec. for R	nected with meter eter disk	inual	
Electrical	R T E	Transformers con = Revolutions of me = Time in Sec. for R = Voltage per Leg a	nected with meter eter disk upplied to motor	nua	
Electrical	R T	Transformers con = Revolutions of me = Time in Sec. for R	nected with meter eter disk applied to motor applied to motor	intra	
Electrical	R T E I	Transformers con = Revolutions of me = Time in Sec. for R = Voltage per Leg a = Amperes per Leg = Power factor of m	nected with meter eter disk applied to motor applied to motor		
Electrical	R T E I PF	Transformers con = Revolutions of me = Time in Sec. for R = Voltage per Leg a = Amperes per Leg = Power factor of m = Factor for 3-phase x I.H.P. = 1.732 x E x I x I	nected with meter eter disk applied to motor applied to motor otor e motors. This reduces to 1 for single phase r PF KW-Hrs. Per 1000 Gallons of = HD in ft. >	notors (0.00315	
Electrical	R T E I PF 1.732 Kilowatt input to Motor = .746	Transformers con = Revolutions of me = Time in Sec. for R = Voltage per Leg a = Amperes per Leg = Power factor of m = Factor for 3-phase x I.H.P. = 1 <u>.732 x E x I x I</u> 1000	nected with meter eter disk applied to motor applied to motor otor e motors. This reduces to 1 for single phase r PF KW-Hrs. Per 1000 Gallons of Cold Water Pumped Per Hour = HD in ft. 2 Pump Eff.	notors (0.00315	
Electrical	R T E I PF 1.732 Kilowatt input to Motor = .746 (1) Thrust Bearing Loss = .0075	Transformers con = Revolutions of me = Time in Sec. for R = Voltage per Leg a = Amperes per Leg = Power factor of m = Factor for 3-phase x I.H.P. = 1.732 x E x I x I 1000 HP per 100 RPM per 10	nected with meter eter disk applied to motor applied to motor otor e motors. This reduces to 1 for single phase r PF KW-Hrs. Per 1000 Gallons of Cold Water Pumped Per Hour = HD in ft. 2 Pump Eff.	notors (0.00315	
	R T E I PF 1.732 Kilowatt input to Motor = .746 (1) Thrust Bearing Loss = .0075 (2) Overall Plant Efficiency some	Transformers con = Revolutions of me = Time in Sec. for R = Voltage per Leg a = Amperes per Leg = Power factor of m = Factor for 3-phase x I.H.P. = 1.732 x E x I x I 1000 HP per 100 RPM per 10 etimes referred to as "Wire factor of the second se	nected with meter eter disk applied to motor applied to motor otor e motors. This reduces to 1 for single phase r PF KW-Hrs. Per 1000 Gallons of Cold Water Pumped Per Hour = HD in ft. 2 Pump Eff.	notors (0.00315	
Electrical	R T E I PF 1.732 Kilowatt input to Motor = .746 (1) Thrust Bearing Loss = .0075 (2) Overall Plant Efficiency some *Thrust (in Ibs.) = (thrust cons	Transformers con = Revolutions of me = Time in Sec. for R = Voltage per Leg a = Amperes per Leg = Power factor of m = Factor for 3-phase x I.H.P. = $1.732 \times E \times I \times I$ 1000 HP per 100 RPM per 10 etimes referred to as "Wire tant (k) laboratory head) from curve sheets	nected with meter ater disk applied to motor applied to motor otor e motors. This reduces to 1 for single phase r PF KW-Hrs. Per 1000 Gallons of Cold Water Pumped Per Hour = HD in ft. > Pump Eff. 1000 lbs. thrust.* to Water" Efficiency + (setting in feet x shaft wt. per ft.)	notors (0.00315	

SUMP PUMP TYPICAL INSTALLATIONS



Typical Pump Installation in Sump

EFFLUENT AND SEWAGE PUMPS TYPICAL INSTALLATIONS



Goulds Water Technology, Bell & Gossett, Red Jacket Series, CentriPro

Suggested Pump Positioning in Sump

VARIABLE SPEED DRIVES

WASTEWATER PUMPS AND VARIABLE SPEED DRIVES

It is acceptable and increasingly more common to operate three-phase wastewater pumps using VFD's or variable frequency (speed) drives. We have successfully tested and operated all our premium cast iron construction, three-phase pumps between 30 and 60 hertz operation. The pumps should never be operated below 30 hertz (the VFD must be programmed for a minimum speed of 30 hertz to prevent continuous operation) or above 60 hertz due to increased motor HP loading, higher amperage and the resultant heat rise (see HP in 70 hertz Performance Multipliers).

The "Affinity Laws" state that for a given pump, the capacity will vary directly with a change in speed, the head will vary as the square of the speed change and the required power will vary as the cube of the speed change. (The Affinity Law formulas can be found in the Water Products Technical Manual, TTECHWP). The Performance Multiplier Chart provides shortcut multipliers that eliminate having to solve the Affinity Law equations.

To calculate a pump's total performance range when using a VFD, use the 30 hertz data to create a minimum speed curve, the VFD controlled pump should always be operated between 30 hertz and the published 60 hertz curve. Where it operates at any given moment is irrelevant.

 Q_1 , H_1 and BHP_1 are determined at the pump's rated speed N₁ (rpm).

 Q_2 , H_2 and BHP_2 are determined at speed N_2 (rpm).

Use the multipliers with a minimum of 3 data points taken from any standard, 60 Hz curve to determine the performance of that pump at a new speed.

Performance Multipliers Hertz

$H_2 = H_1 \times 1.37$	$BHP_2 = BHP_1 \times 1.6$
d published curve	e data
$H_2 = H_1 x .69$	$BHP_2 = BHP_1 \times .57$
$H_2 = H_1 x .45$	$BHP_2 = BHP_1 \times .3$
$H_2 = H_1 \underline{x.25}$	$BHP_2 = BHP_1 \underline{x .125}$
	d published curve $H_2 = H_1 \times .69$ $H_2 = H_1 \times .45$

An example would be, solve for Q_2 , H_2 and BHP_2 for a 60 Hz pump that produces 100 gpm (Q_1) @ 100' tdh (H_1) using 5 hp (BHP₁) when it is operated at 30 Hz : **Answers:** 100 gpm <u>x .5</u> = 50 gpm, 100' TDH <u>x .25</u> = $25' \text{ TDH and } 5 \text{ hp } \underline{x.125} = .63 \text{ hp.}$

VFD's save energy while reducing the thrust on the motor bearings and the starting torgue on the shaft and impeller.

Contact Customer Service for details, pricing and availability of our full line of VFD products.

STANDARD PANEL SELECTION CHECK LIST

PANEL SIZING

Pump Model Chosen: ____ 1. Phase: Single_____ Three_____ (found on bulletin) 2. Amp draw of pump: -3. Simplex ("1" Pump) _____ Duplex ("2" Pumps in Pit) _____ 4. Does pump have a seal fail circuit: yes or no (see note) (NOTE: If Question 4 is yes, add a seal fail option as noted.) If Question 1. Single 3. Simplex use Chart A If Question 1. Three 3. Simplex use Chart B If Question 1. Single 3. Duplex use Chart C If Question 1. Three 3. Duplex use Chart D

CHART A

Panel Part Number	Amp / Maximum HP	Enclosure
S10020N1 (non-modifiable)	up to 20	Indoor
S10020	up to 20	
S12127	21-27	
S12836	28-36	
S1GD2 (includes caps for 1GD,12GDS after 12/2005)	2 HP	Indoor/
S1FGC2 (use with1GA/15GDS)	3 HP	Outdoor
S1FGC3 (use with1/2GA/15/20GDS)	5.4 HP	
S1FGC5 (use with 2GA /20GDS)	9.4 HP	

Add option H for seal fail circuit to all of the above except S10020N1. Except for GA/GDS grinder pumps, seal fail and high temperature are included in panel.

Goulds Water Technology, Bell & Gossett, Red Jacket Series, CentriPro

CHART B

Panel Part Number	Amp / Maximum HP	Enclosure
S31625	1.6-2.5	
S32540	2.5-4.0	
S34063	4.0-6.3	
S36310	6.3-10	Indoor /
S31016	10-16	Outdoor
S31620	16-20	
S32025	20-25	
S32232	22-32	

Add option H for seal fail circuit to all of the above, unless using a GA/GDS pump, use an "O" option.

CHART C

Panel Part Number	Amp / Maximum HP	Enclosure
D10020N1	up to 20	Indoor
D10020	up to 20	
D12127	21-27	
D12836	28-36	
D1GD2 (includes caps for 1GD,12GDS after 12/2005)	2 HP	Indoor /
D1FGC2 (use with 1GA / 15GDS)	3 HP	Outdoor
D1FGC3 (use with 1/2GA / 15/20GDS)	5.4 HP	
D1FGC5 (use with 2GA / 20GDS)	9.4 HP	

Add option J for seal fail circuit to all of the above except D10020N1. Do not add seal fail for GA/GDS grinder pumps, seal fail and high temperature are included in panel.

CHART D

Panel Part Number	Amp / Maximum HP	Enclosure
D31625	1.6-2.5	
D32540	2.5-4.0	
D34063	4.0-6.3	
D36310	6.3-10	Indoor /
D31016	10-16	Outdoor
D31620	16-20	
D32025	20-25	
D32232	22-32	

Add option J for seal fail circuit to all of the above except for GA/ GDS pumps, use an Option "P". For other panel options see catalog for adders. For adders not found in the catalog, or more than three options a specification is needed for the Customer Service Department to prepare a quotation. Use of the Custom panel selection sheet is advised with more than three options.

Goulds Water Technology, Bell & Gossett, Red Jacket Series, CentriPro

Wastewater

1 FOR SEPARATE 120 VAC

TERMINALS (H) AND (L1).

CONNECT 15 AMP MAX.

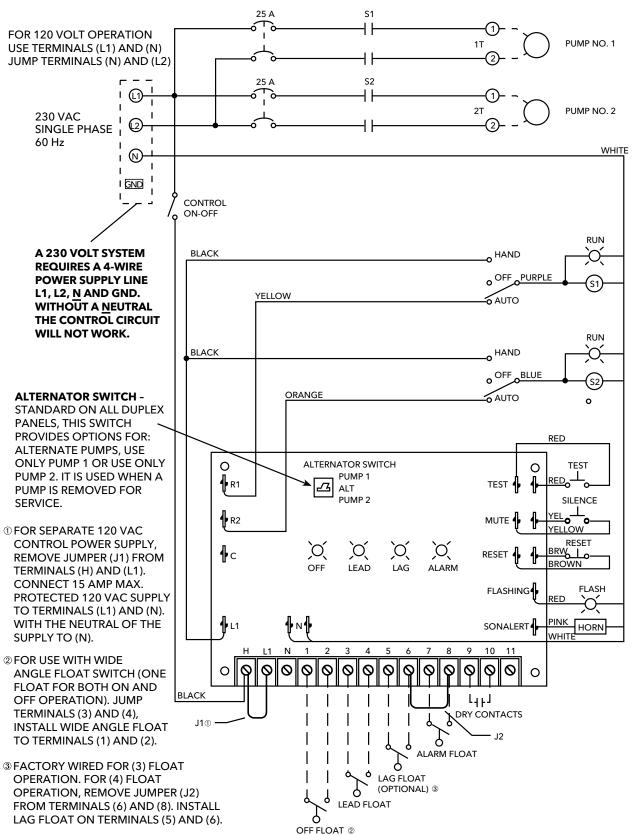
TERMINALS (5) AND (6).

60 Hz

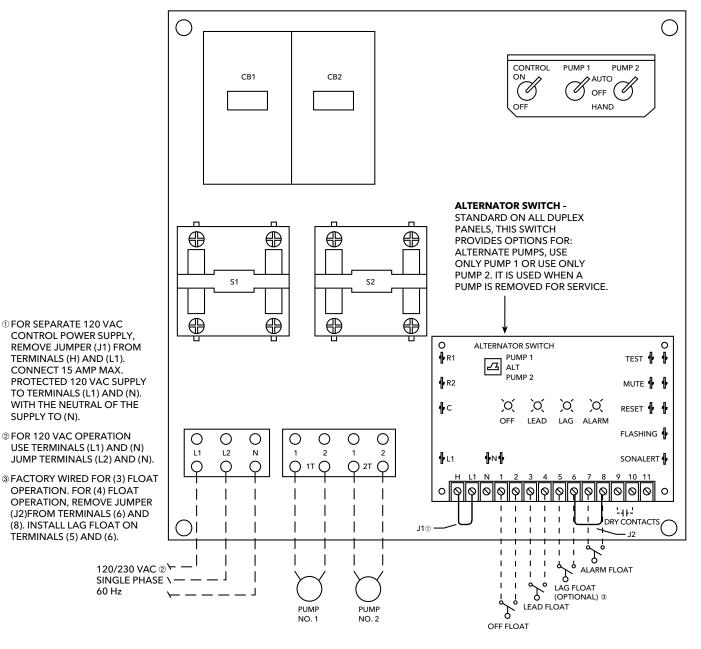
SUPPLY TO (N).

DUPLEX SINGLE PHASE WIRING DIAGRAM - D10020

NOTE: The standard panels shown in this book are not designed to be used with pumps requiring external capacitors. See the catalog for panels with built-in capacitor packs.



DUPLEX SINGLE PHASE PANEL LAYOUT - D10020

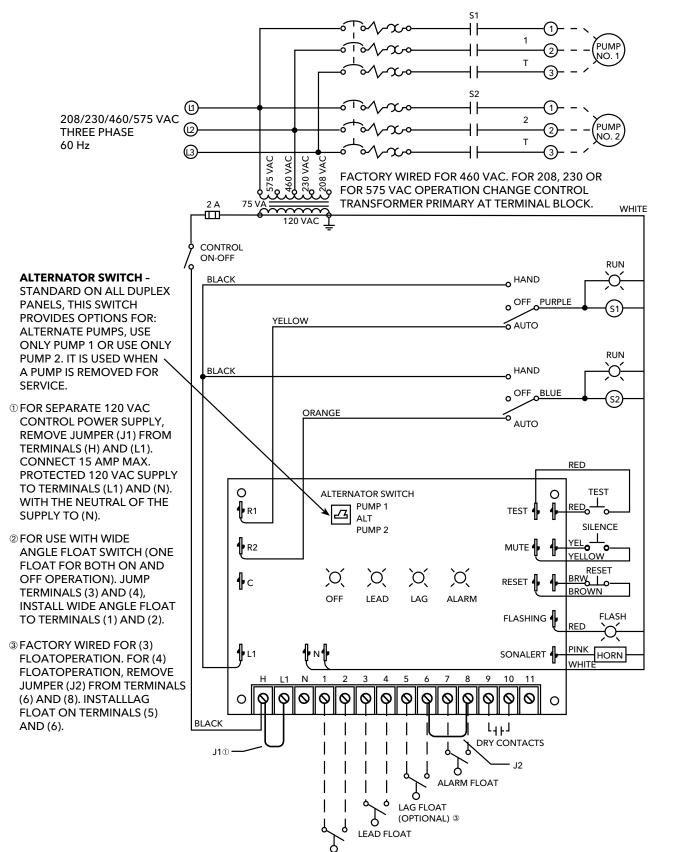


NOTE: Panel is not to be used with pumps that do not include capacitors.

Goulds Water Technology, Bell & Gossett, Red Jacket Series, CentriPro

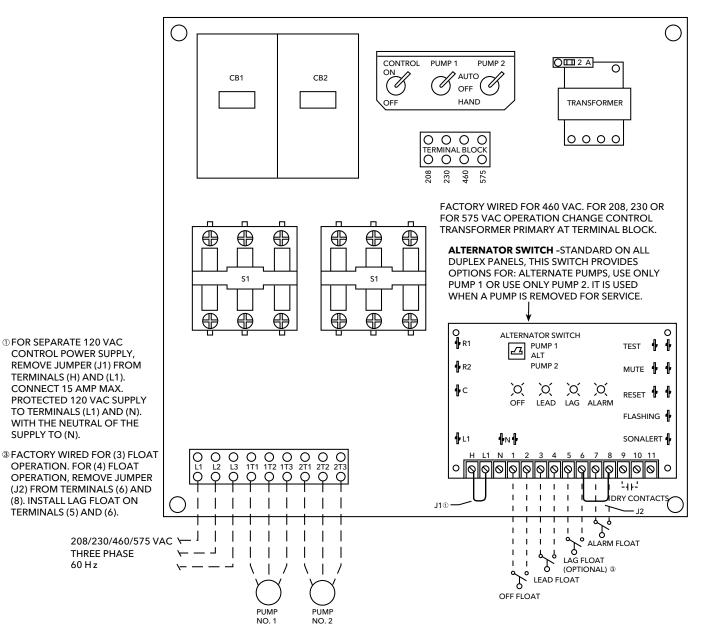
SUPPLY TO (N).

DUPLEX THREE PHASE WIRING DIAGRAM - D3 - - - -



OFF FLOAT @

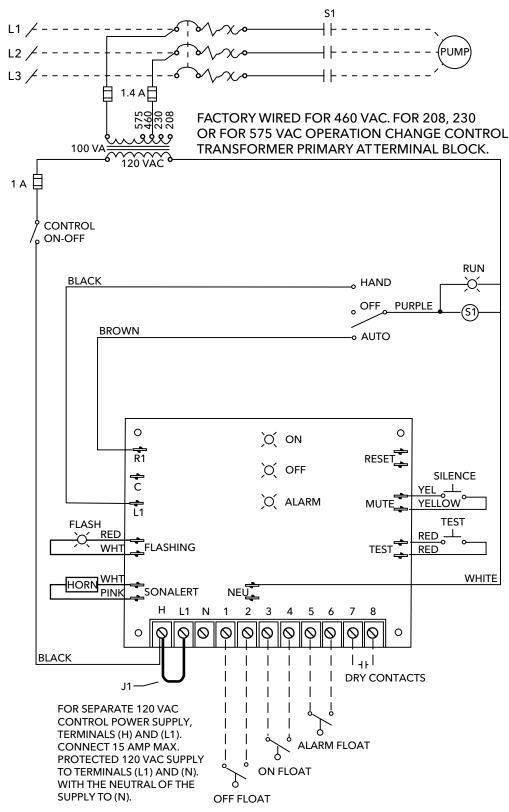
DUPLEX THREE PHASE PANEL LAYOUT - D3 - - -



Goulds Water Technology, Bell & Gossett, Red Jacket Series, CentriPro

SIMPLEX THREE PHASE PANEL LAYOUT

NOTE: A fused disconnect or circuit breaker must be provided by installer. Provide disconnect sizing per NEC 430-53(C).



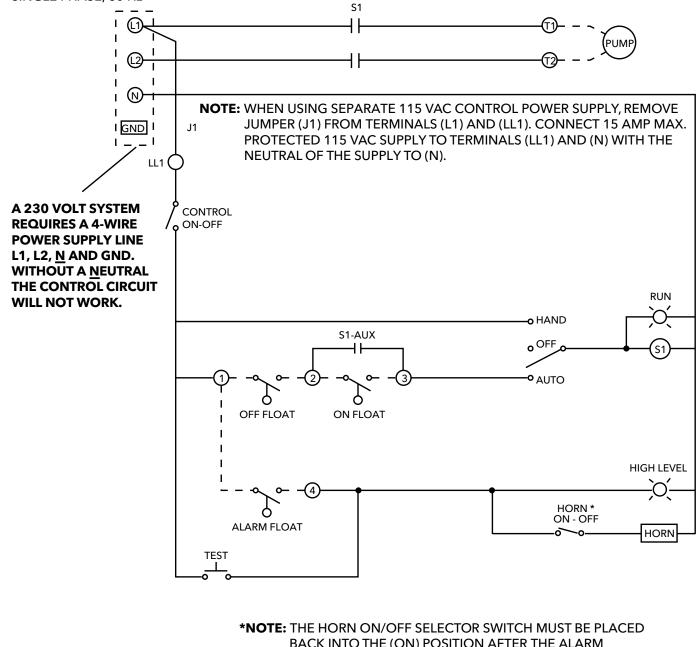
FOR USE WITH WIDE ANGLE FLOAT SWITCH (ONE FLOAT FOR BOTH ON AND OFF OPERATION). JUMP TERMINALS (3) AND (4), INSTALL WIDE ANGLE FLOAT TO TERMINALS (1) AND (2).

Wastewater

SIMPLEX SINGLE PHASE WIRING DIAGRAM - S10020 Before October 1, 2003

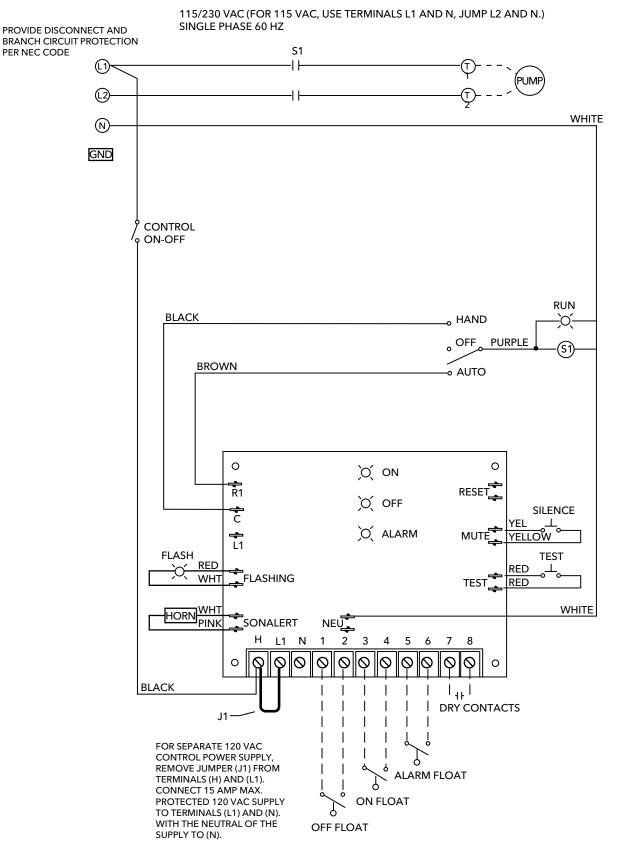
NOTE: The standard panels shown in this book are not designed to be used with pumps requiring external capacitors. See the catalog for panels with built-in capacitor packs.

115/230 VAC (FOR 115 VAC, USE TERMINALS L1 AND N, JUMP L2 AND N). SINGLE PHASE, 60 Hz



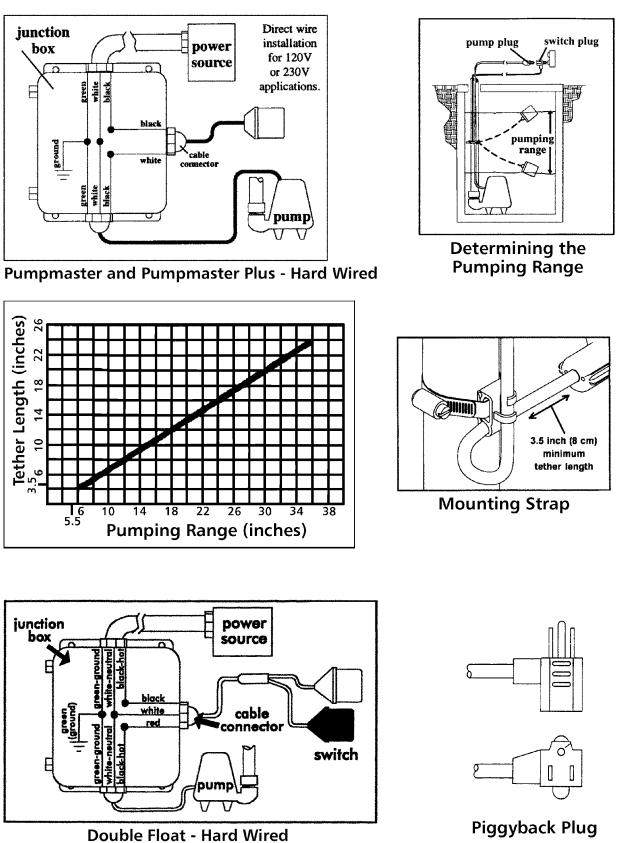
BACK INTO THE (ON) POSITION AFTER THE ALARM CONDITION HAS BEEN CORRECTED IN ORDER TO MAINTAIN THE AUDIO ALARM ANNUNCIATION.

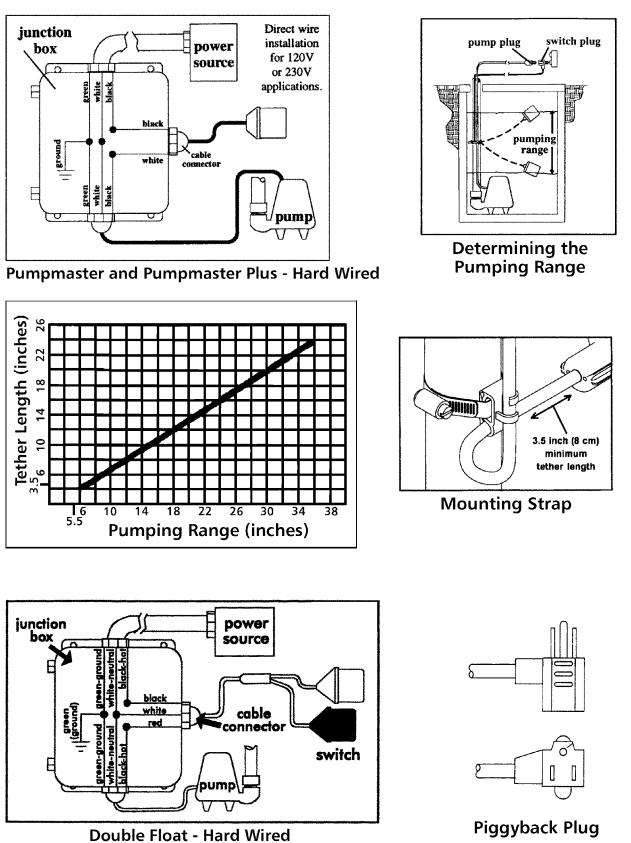
SIMPLEX SINGLE PHASE WIRING DIAGRAM - S10020 After October 1, 2003

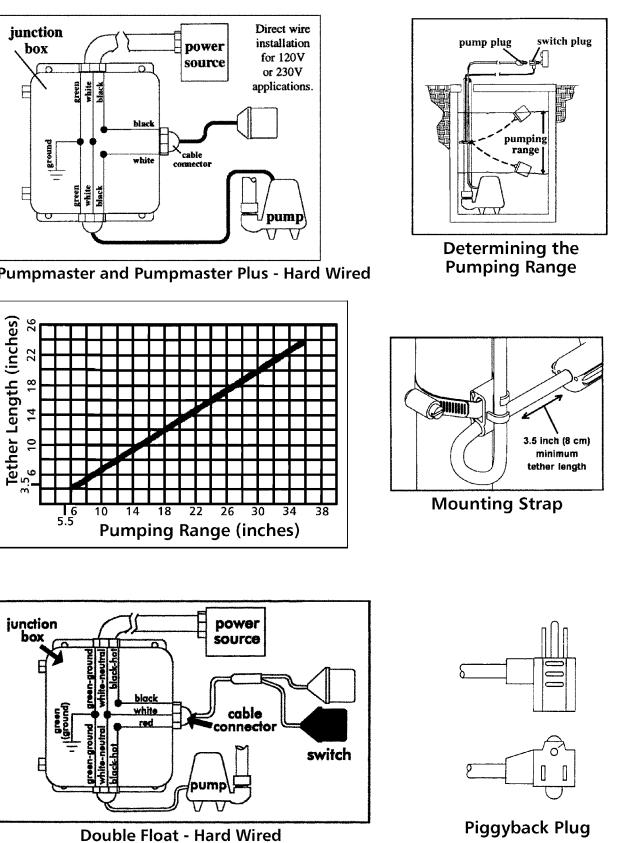


FOR USE WITH WIDE ANGLE FLOAT SWITCH (ONE FLOAT FOR BOTH ON AND OFF OPERATION). JUMP TERMINALS (3) AND (4), INSTALL WIDE ANGLE FLOAT TO TERMINALS (1) AND (2).

SWITCH DIAGRAMS







SEWAGE CONTROL PANELS AND SWITCHES

There are two basic switches used in sewage and effluent systems. Single-action or narrow-angle float switches perform one function (on or off). They operate over a range of 15°. Wide-angle, or double-action float and diaphragm switches perform two functions (on and off). Wide-angle float switches operate over a 90° range and diaphragm switches on a 6" rise in water level.

Control panel wiring diagrams refer to 3 float and 4 float systems, this terminology refers to the use of singleaction switches. The following chart shows how many of either type switch to use with different control panels.

Duplex Control Panels

Typical Duplex panels use the following switch set-ups depending on the switch type you use. Most Duplex control panels have a standard high level alarm circuit with a flashing light, most have a horn or bell. Once it turns On - the alarm must be manually reset (turned off) on Duplex panels.

Using a Single-action or Narrow-angle Switch requires:

Three Float Panel Wiring		Four Float Panel Wiring	
#1 Bottom	Pumps Off	#1 Bottom	Pumps Off
#2 Middle	1st Pump On	#2 2nd	1st Pump On
#3 Тор	2nd Pump & Alarm On	#3 3rd	2nd Pump On
		#4 Top	Alarm On

Using Double-Action or Wide-Angle Switches; A2D23W, A2E21, A2E22, A2E23, A2D11, A2D31 or A2S23 requires:

Three Float Panel Wiring Four Float Panel Wiring #1 Bottom 1st Pump On/Both Off 1st Pump On/Both Off #1 Bottom 2nd Pump On #2 Top 2nd Pump and Alarm On #2 Middle Alarm On #3 Top

Simplex Control Panels

Only some Simplex panels have alarms. This is why the switch quantity requirements vary by simplex panel model. All of our SES panels have high level alarms.

Using a Single-action or Narrow-angle Switch requires:

Simplex Panel with Alarm		<u>Simplex Pa</u>	Simplex Panel with No Alarm		
#1 Bottom	Pump Off	#1 Bottom	Pump Off		
#2 Middle	Pump On	#2 Тор	Pump On		
#3 Top	Alarm On/Off				

Using Double-Action or Wide-angle Switches requires:

Simplex Panel with Alarm		Simplex Panel with No Alarm		
#1 Bottom	Pump On/Off	#1 Bottom	Pump On/Off	

NOTE: 1st pump may also be referred to as "Lead" pump, 2nd pump may be called "Lag" pump.

Alarm On/Off

Wastewater

Brochure (BCPFS) found at www.xylem.com/BCPFS.

#2 Top

We sell and stock a complete line of wastewater float switches. The most upto-date information is found in the Pump/Control/Panel Switches Technical

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Wastewater

NOTES

NOTES

Xylem |'zīləm|

The tissue in plants that brings water upward from the roots;
 a leading global water technology company.

We're a global team unified in a common purpose: creating advanced technology solutions to the world's water challenges. Developing new technologies that will improve the way water is used, conserved, and re-used in the future is central to our work. Our products and services move, treat, analyze, monitor and return water to the environment, in public utility, industrial, residential and commercial building services settings. Xylem also provides a leading portfolio of smart metering, network technologies and advanced analytics solutions for water, electric and gas utilities. In more than 150 countries, we have strong, long-standing relationships with customers who know us for our powerful combination of leading product brands and applications expertise with a strong focus on developing comprehensive, sustainable solutions.

For more information on how Xylem can help you, go to www.xylem.com



Xylem Inc. 2881 East Bayard Street Ext., Suite A Seneca Falls, NY 13148 Phone: (866) 325-4210 Fax: (888) 322-5877 www.xylem.com

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